

FAN ENGINEERING WEALTH GUIDE

Fan Engineering Wealth Guide

PART I

Ventech Systems Private Limited

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INDEX

- Abbreviations, Fan Terminology and Definitions
- Formulas For Fan Applications
- How to Use the Fan Laws for Performance Changes
- Performance Correction for Temperature & Altitude
- How to Convert the Fan's Performance to Standard Conditions
- Capture velocities (or Airflow) For Exhaust Hoods
- Air Change Rates for ventilation
- velocity-to-velocity Pressure Conversion Chart
- Definitions of English & Metric Units
- Pressure Equivalent Chart
- English & Metric Conversions
- Friction Loss Per 100 Feet of Round Duct
- Area and Circumference of Circles
- Gauges & Equivalent Metal Thickness
- Fractions to Equivalent Decimal values

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Abbreviations, Fan Terminology and Definitions

- ARR.** Arrangement of fan.
- BHP** Brake horsepower, the fan's power consumption.
- CCW** Counterclockwise. Used to describe the rotation of an impeller. Rotation is determined by viewing the impeller from the drive side on centrifugal fans. Determining the rotation is not a factor on axial and inline centrifugal fans.
- CFM** Cubic feet per minute, the volume of air moved per minute.
- CL** Class of fan. The class identifies the limit of the fan's performance range.
- CW** Clockwise. Used to describe the rotation of an impeller. Rotation is determined by viewing the impeller from the drive side on centrifugal fans.
- dBA** Estimated sound pressure level in the space using "A" weighting.
- DWDI** Double width double inlet.
- EFFICIENCY** A Ratio of the useful energy (work) provided by a system to the energy supplied to it. Used to provide a relative performance comparison of fans.
- FPM** Feet per minute, the velocity of the airstream.
- HP** Horsepower, the fan's motor size.
- I.D.** Inside diameter of fan, duct or transition.
- Lp** Sound Pressure Level. Describes the loudness level of the sound, like the brightness level of a light bulb. This value varies with the distance from the sound source and the environment surrounding the sound source. Sound pressure is usually expressed in decibels with a reference level to 0.0002 microbars.
- Lw** Sound Power Level. Describes the total amount of acoustical energy the fan emits, like the watt rating of a light bulb describes the total amount of energy the light emits. This value is independent of location, distance, and environment. Sound power is usually expressed in decibels with a reference level to 10^{-12} watts.
- LwA** Sound Power Level 'A' weighted. This is a single value representing the fan's overall sound power level. 'A' weighting adjusts the sound power level for the response of the human ear. This value is often used in the calculation of sound pressure levels.
- ME** Mechanical efficiency (or Total efficiency). Mechanical efficiency is a ratio of the total fan power output to the power supplied to the fan. Mechanical efficiency uses total pressure, which includes the kinetic energy, to calculate the efficiency.
- O.D.** Outside diameter of fan, duct or transition.
- OV** Outlet velocity, the average air velocity at the outlet of the fan. Outlet velocity is calculated by dividing the CFM by outlet area.
- RPM** Revolutions per minute, the number of rotations the fan shaft makes per minute.
- SE** Static efficiency. Static efficiency is a ratio of the fan power output to the power supplied to the fan. Static efficiency uses static pressure, which does not include the kinetic energy, to calculate the efficiency. It can be found by multiplying the Mechanical efficiency by the ratio of the fan static pressure to the fan total pressure.
- SP** Static pressure is the measure of the potential energy of the airstream. SP acts equally in all directions. It is this pressure in the duct that tends to burst or collapse the duct.
- SWSI** Single width single inlet.
- TP** Total pressure, the measure of the energy content of the airstream. It is the sum of static pressure (SP) and velocity pressure (VP).
- TS** Tip speed, the speed of the fan blade tip.
- VP** Velocity pressure, the measure of the energy content of the airstream. Velocity pressure acts in the direction of

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the airflow. It is the pressure necessary to accelerate the air.

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Formulas For Fan Applications

$$\text{Mechanical Efficiency, ME} = \frac{\text{CFM} \times \text{TP} \times K_p}{6343.3 \times \text{BHP}} \times 100$$

$$\text{Static Efficiency, SE} = \frac{\text{CFM} \times \text{SP} \times K_p}{6343.3 \times \text{BHP}} \times 100$$

(where SP is in inches H₂O)

$$\text{Total Pressure, TP} = \text{SP} + \text{VP}$$

$$\text{Velocity, V} = \frac{\text{CFM}}{\text{Area in Sq. Ft.}}$$

$$\text{Velocity Pressure, VP} = \left(\frac{V}{1097.8} \right)^2 \times \text{density in pounds per cubic foot}$$

If the density is 0.075 lbs/ft³, the equation for VP reduces to = (V/4008.6)²

$$K_p = \left(\frac{\ln(1+z)}{\ln(1+z)} \right)^x$$

$$x = \text{Pe}_1 + 13.595 \times \text{P}_b$$

$$z = \left(\frac{y+1}{\frac{6343.3 \times \text{BHP}}{\text{CFM}}} \right)^{\frac{1}{\text{Pe}_1 + 13.595 \times \text{P}_b}}$$

P_t = Total Pressure @ fan's inlet in in-wg

P_b = Barometric Pressure in in-Hgz

SYSTEM CURVE EQUATION

The following formula is used to find other points on the system line when SP₁ and CFM₁ are known. Most, but not all, systems follow this relationship.

$$\text{SP}_2 = \text{SP}_1 \left(\frac{\text{CFM}_2}{\text{CFM}_1} \right)^2$$

How to Use the Fan Laws for Performance Changes

There are two reasons why a fan's performance may need to be changed:

- The system or area requires additional airflow (CFM).
- The actual system static pressure (SP) is different from the design value.

When these situations occur, it is important to understand how they can affect the fan's performance.

The effect on the fan's performance can be shown by using the Fan Laws, shown below.

3. After installing the fan, the Plant Manager wants to increase the airflow into the plant to 41,500 CFM. The fan laws are used to determine how this fan will be affected by the new system requirements.

4. The known values are

$$\begin{aligned} \text{CFM}_1 &= 33,120 \text{ CFM} & \text{SP}_1 &= 2.5" \text{ SP} \\ \text{CFM}_2 &= 41,500 \text{ CFM} & \text{RPM}_1 &= 620 \text{ RPM} \\ \text{BHP}_1 &= 20.01 \text{ BHP} \end{aligned}$$

5. The unknown values are

$$\begin{aligned} \text{RPM}_2 &= ?? \\ \text{SP}_2 &= ?? \\ \text{BHP}_2 &= ?? \end{aligned}$$

6. Using the fan law equations, the unknown values are calculated as follows

$$\text{RPM}_2 = \frac{41,500}{33,120} \times 620 = 777 \text{ RPM}_2$$

FAN LAW EQUATIONS

$$\text{CFM}_2 = \frac{\text{RPM}_2}{\text{RPM}_1} \times \text{CFM}_1$$

$$\text{SP}_2 = \left(\frac{\text{RPM}_2}{\text{RPM}_1} \right)^2 \times \text{SP}_1$$

$$\text{BHP}_2 = \left(\frac{\text{RPM}_2}{\text{RPM}_1} \right)^3 \times \text{BHP}_1$$

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Subscript 1 = existing conditions

Subscript 2 = new conditions

EXAMPLE

1. Assume a customer requires a fan to operate at 33,120

$$\frac{SP_2}{SP_1} = \left(\frac{RPM_2}{RPM_1}\right)^2 \times 2.5" = 3.93"$$

$$BHP_2 = \left(\frac{RPM_2}{RPM_1}\right)^3 \times 20.01 =$$

7. What does this information tell us?

In order to use the same fan for an airflow of 41,500 CFM, the RPM needs to be increased to 777 RPM.

The new performance increases the fan's horsepower requirement from 25 HP to 50 HP. If the fan is sped up to 777 RPM the motor must be resized.

IMPORTANT NOTE: The new RPM should be checked to make sure it does not exceed the maximum allowable RPM for the fan that is installed. If this information is not provided in the catalog or you would like **VENTECH SYSTEMS PVT. LTD.** to review the application, please contact us.

39.39 BHP₂

2. CFM at 2.5" SP, at standard air density. Per the specifications, a BC backward inclined fan is required.
3. Based on the above information, VSPL engineer selects a suitable fan, which will operate at 620 RPM and 20.01 BHP to meet the required performance.

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Performance Correction for Temperature & Altitude

In each fan catalog the performance tables are based on standard air density, which is defined as dry air at 70°F at sea level (29.92 Hg barometric pressure). This is equal to 0.075 lb./ft³ density. The fan performance tables provide the fan RPM and brake horsepower requirements for the given CFM and static pressure, at standard air density.

When the fan performance is not at standard conditions, the performance must be converted to standard conditions before entering the fan performance tables. The fan performance is converted to standard conditions by using the correction factor in the Temperature and Altitude Correction Chart shown below.

The following are examples explaining how to convert the fan's performance to standard conditions.

Temperature and Altitude Correction Factors

| AIR TEMP °F | ALTITUDE IN FEET ABOVE SEA LEVEL | | | | | | | | | | | |
|-------------|--|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | 0 | 1000 | 2000 | 3000 | 4000 | 5000 | 6000 | 7000 | 8000 | 9000 | 10000 | 15000 |
| | BAROMETRIC PRESSURE IN INCHES OF MERCURY | | | | | | | | | | | |
| | 29.92 | 28.86 | 27.82 | 26.82 | 25.84 | 24.90 | 23.98 | 23.09 | 22.22 | 21.39 | 20.58 | 16.89 |
| -50 | 1.293 | 1.247 | 1.201 | 1.159 | 1.116 | 1.076 | 1.036 | .997 | .960 | .924 | .889 | .729 |
| 0 | 1.152 | 1.111 | 1.071 | 1.032 | .995 | .959 | .923 | .889 | .856 | .824 | .792 | .650 |
| 50 | 1.039 | 1.003 | .967 | .932 | .897 | .864 | .833 | .801 | .772 | .743 | .715 | .586 |
| 70 | 1.000 | .964 | .930 | .896 | .864 | .832 | .801 | .772 | .743 | .714 | .688 | .564 |
| 100 | .946 | .912 | .880 | .848 | .818 | .787 | .758 | .730 | .703 | .676 | .651 | .534 |
| 150 | .869 | .838 | .808 | .770 | .751 | .723 | .696 | .671 | .646 | .620 | .598 | .490 |
| 200 | .803 | .774 | .747 | .720 | .694 | .668 | .643 | .620 | .596 | .573 | .552 | .453 |
| 250 | .747 | .720 | .694 | .669 | .645 | .622 | .598 | .576 | .555 | .533 | .514 | .421 |
| 300 | .697 | .672 | .648 | .624 | .604 | .580 | .558 | .538 | .518 | .498 | .480 | .393 |
| 350 | .654 | .631 | .608 | .586 | .565 | .544 | .524 | .505 | .486 | .467 | .450 | .369 |
| 400 | .616 | .594 | .573 | .552 | .532 | .513 | .493 | .476 | .458 | .440 | .424 | .347 |
| 450 | .582 | .561 | .542 | .522 | .503 | .484 | .466 | .449 | .433 | .416 | .401 | .328 |
| 500 | .552 | .532 | .513 | .495 | .477 | .459 | .442 | .426 | .410 | .394 | .380 | .311 |
| 550 | .525 | .506 | .488 | .470 | .454 | .437 | .421 | .405 | .390 | .375 | .361 | .296 |
| 600 | .500 | .482 | .465 | .448 | .432 | .416 | .400 | .386 | .372 | .352 | .344 | .282 |
| 650 | .477 | .460 | .444 | .427 | .412 | .397 | .382 | .368 | .354 | .341 | .328 | .269 |
| 700 | .457 | .441 | .425 | .410 | .395 | .380 | .366 | .353 | .340 | .326 | .315 | .258 |
| 750 | .439 | .423 | .407 | .393 | .379 | .365 | .351 | .338 | .326 | .313 | .303 | .248 |
| 800 | .420 | .404 | .389 | .375 | .362 | .350 | .336 | .323 | .311 | .300 | .290 | .237 |
| 850 | .404 | .391 | .376 | .363 | .349 | .336 | .324 | .312 | .300 | .289 | .279 | .228 |
| 900 | .389 | .376 | .363 | .349 | .336 | .324 | .312 | .300 | .289 | .279 | .268 | .220 |
| 950 | .376 | .363 | .350 | .337 | .325 | .313 | .301 | .290 | .279 | .269 | .259 | .212 |
| 1000 | .363 | .350 | .338 | .325 | .314 | .302 | .291 | .280 | .270 | .259 | .250 | .205 |

How to Convert the Fan's Performance to Standard Conditions

When Operating Conditions Are Known:

Assume, SWSI fan is to handle 17,000 CFM, 2.5" SP, at 300°F and 3000 ft. altitude. This fan is not operating at standard conditions; therefore, the performance needs to be converted to standard conditions to find the fan's speed and brake horsepower. The fan's performance is converted to standard conditions as follows:

17,620 – 16,850

929 – 915

1. From the table above, the correction factor for 300°F and 3000 ft. altitude is 0.624.
2. The static pressure, at standard air density, is calculated by dividing the operating SP by the correction factor; i.e., $2.5" \div .624 = 4"$ SP. The static pressure is 4" at standard air density.
3. Knowing the CFM and the static pressure, at standard air density, the fan RPM and BHP can be found. SWSI fan performance table with 17,000 CFM and 4" SP.
4. In this example, the RPM and BHP are between the values listed in the performance table; therefore, the RPM and BHP are determined by interpolation. The RPM is determined by the following equation

$$\frac{17,000 - 16,850}{17,620 - 16,850} = \frac{\text{RPM} - 915}{929 - 915}$$

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5. Subtracting the top and bottom values reduces the equation to

$$\frac{150}{=915770} \text{ RPM} \quad 14 \quad =$$

6. Dividing the values on the left side and multiplying each side by 14 reduces the equation to

$$0.19 \times 14 = \text{RPM} - 915$$

7. Multiplying the values on the left side and adding 915 to each side reduces the equation to

$$2.66 + 915 = \text{RPM}$$

8. Solving the left side of the equation results in a fan RPM equal to

$$\text{RPM} = 918 \text{ RPM}$$

9. Next, the BHP is determined by the following equation $17,000 - 16,850$ **BHP** -

$$\frac{14.20}{17,620 - 16,850} \quad 15.03 - 14.20 \quad =$$

10. Subtracting the top and bottom values reduces the equation to

$$\frac{150}{770} \quad \frac{\text{BHP} - 14.20}{0.83} \quad =$$

11. Dividing the values on the left side and multiplying each side by 0.83 reduces the equation to

$$0.19 \times 0.83 = \text{BHP} - 14.20$$

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12. Multiplying the values on the left side and adding 14.20 to each side reduces the equation to

$$0.16 + 14.20 = \text{BHP}$$

13. Solving the left side of the equation results in a fan BHP equal to

$$\text{BHP} = 14.36 \text{ BHP}$$

Conclusions — For this example, the required fan RPM is 918 RPM and the brake horsepower at standard conditions is 14.36 BHP. The brake horsepower, 14.36 BHP at standard conditions (70°F at sea level), is also referred to as the cold or starting brake horsepower.

If the fan is installed at a higher altitude than sea level, such as described in this example, the cold or starting brake horsepower at that altitude is determined by the following equation:

$$\text{Cold BHP at altitude} = \text{BHP}_{\text{std}} \times \text{Correction Factor at Required Elevation and } 70^{\circ}\text{F}$$

For this example, the cold or starting brake horsepower at 3000 ft. altitude and 70°F is

$$14.36 \times 0.896 = 12.87 \text{ BHP, cold BHP @ 3000 ft. altitude}$$

To determine the BHP at operating conditions, 300°F and 3000 ft. altitude, multiply the BHP at standard conditions by the factor for these conditions:

$$14.36 \times 0.624 = 8.96 \text{ BHP at operating conditions, } 300^{\circ}\text{F and } 3000 \text{ ft. altitude}$$

The fan performance information for 17000 CFM, 2.5" SP, at 300°F and 3000 ft. altitude is

- 918 RPM
- 8.96 BHP at operating conditions (300°F and 3000 ft. altitude)
- 12.87 BHP (cold BHP, 70°F and 3000 ft. altitude)
- 14.36 BHP at standard conditions or cold BHP at 70°F and sea level
- 4" SP at standard conditions

When Operating Density Is Known:

Assume a SWSI fan suitable for handling 23,500 CFM, 3.0" SP, at 0.06364 lb./ft³. This fan is not operating at standard conditions; therefore, the performance needs to be converted to standard conditions to find the fan's speed and brake horsepower. The fan's performance is converted to standard conditions as follows:

1. Using the operating density of 0.06364 lb./ft³, the correction factor is determined by dividing the operating density by the standard density, 0.075 lb./ft³.

$$\text{Correction Factor} = \frac{\text{Operating Density}}{\text{Standard Density}} = .848$$

2. The static pressure at standard air density is calculated by dividing the operating SP by the conversion factor, i.e., 3.0" ÷ .848 = 3.5" SP. The static pressure is 3.5" at standard air density.
3. Knowing the CFM and the static pressure at standard air density, the fan RPM and BHP can be found. Enter the 365 BC, SWSI fan performance table (Bulletin 300) with 23,500 CFM and 3.5" SP.
4. This example also finds the RPM and BHP between the values listed in the performance table; therefore, the RPM and BHP are determined by interpolation.
5. The RPM is determined by the following equation

$$\frac{23,500 - 22,980}{24,510 - 22,980} = \frac{\text{RPM} - 1015}{1054 - 1015}$$

6. Subtracting the top and bottom values reduces the equation to

$$\frac{520}{1530} = \frac{\text{RPM} - 1015}{39}$$

7. Dividing the values on the left side and multiplying each side by 39 reduces the equation to

9. Solving the left side of the equation results in a fan RPM equal to

$$\text{RPM} = 1028 \text{ RPM}$$

10. Next, the BHP is determined by the following equation,

$$\frac{23,500 - 22,980}{24,510 - 22,980} = \frac{\text{BHP} - 20.15}{22.48 - 20.15}$$

11. Subtracting the top and bottom values reduces the equation to

$$\frac{520}{1530} = \frac{\text{BHP} - 20.15}{2.33}$$

$$0.3 \times 39 = \text{RPM} - 1015$$

8. Multiplying the values on the left side and adding 1015 to each side reduces the equation to

$$13 + 1015 = \text{RPM}$$

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12. Dividing the values on the left side and multiplying each side by 2.33 reduces the equation to

$$0.34 \times 2.33 = \mathbf{BHP} - 20.15$$

13. Multiplying the values on the left side and adding 20.15 to each side reduces the equation to

$$0.79 + 20.15 = \mathbf{BHP}$$

14. Solving the left side of the equation results in a fan BHP equal to

$$\mathbf{BHP = 20.94 BHP}$$

Conclusions — For this example, the required fan RPM is 1028 RPM and the brake horsepower is 20.94 BHP at standard conditions. The brake horsepower, 20.94 BHP at standard conditions (70°F at sea level), is also referred to as the cold or starting brake horsepower.

To determine the BHP at operating conditions, multiply the BHP at standard conditions by the conversion factor for these conditions:

$$\mathbf{20.94 \times 0.848 = 17.76 BHP}$$

at operating conditions

The fan performance information for 23,500 CFM, 3.0" SP, at 0.06364 lb./ft³ is

- 1028 RPM
- 17.76 BHP at operating conditions of 0.06364 lb./ft³
- 20.94 BHP at standard conditions (70°F at sea level)
- 3.5" SP at standard conditions.

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Capture velocities (or Airflow) For Exhaust Hoods

Exhaust hoods are critical devices used to protect workers from process fumes or dust. Exhaust hoods induce airflow from the work station to the hood to remove contaminants or particles from the work area. The “capture velocity” is the air velocity required to move the contaminants from the work station to the hood. Capture velocities and hood designs depend on the type of fume or dust being removed. Hood designs include canopy hoods, downdraft hoods, booth-type hoods, slot hoods, etc. The chart at right shows the capture velocity and hood design for a given process.

| PROCESS | TYPE OF HOOD | AIRFLOW OR CAPTURE VELOCITY |
|--|---|---|
| Abrasive Blasting | Down draft Hood Cross draft Hood | 60-100 CFM/ft ² of Floor 100 CFM/ft ² of Wall |
| Auto Parking Garage | 2 Level | 500 CFM/Parking Space |
| Bag Loading for Grain Elevators, Feed Mills, Flour Mills | Canopy Hood | 100 CFM/ft ² Open Face Area 500 FPM Maximum |
| Ceramic: Dry Pan Dry Press | Enclosure Hood Local at Die Local at Die At Supply Bin Booth Hood | 200 FPM Thru All Openings 500 CFM 500 CFM 500 CFM 400 FPM (Face) |
| Spraying (Lead Glaze) | | |
| Cooling Tunnels (Foundry) | Enclosure Hood | 75-100 CFM Per Running Foot of Enclosure |
| Core Sanding (on Lathe) | Downdraft Hood Under Work | 100 FPM at Source |
| Crushers & Grinders | Enclosure Hood | 200 FPM Thru Openings |
| Degreasing; Evaporation From Tanks | Canopy Hood | 50-100 FPM |
| Forge (Hand) | Booth Hood | 200 FPM at Face |
| Furniture Stripping Tank | Slot Hood | 45 CFM/ft ² of Tank Area |
| Metal Cutting Bandsaw | Booth Hood | 225 CFM/ft ² of Open Area |
| Metal Spraying | Booth Hood | a) 150 CFM/ft ² of Face Area, Non-toxic b) 200 CFM/ft ² of Face Area, Toxic |
| Outboard Motor Test Tank | Side Draft Hood | 200 CFM/ft ² of tank openings |
| Packaging Machines | Booth Hood Downdraft Hood Complete Enclosure | 50-100 FPM at Face 95-150 FPM Down 100-400 FPM Opening |
| Paper Machine | Canopy Hood | 200-300 FPM at Face |
| Pickling Metals | Canopy Hood | 200-250 FPM |
| Plating Metals | Canopy Hood | 225-250 FPM |
| Restaurant Range | Hood Against Wall Island Type Hood | 80 CFM/ft ² of Hood Area 125 CFM/ft ² of Hood Area |
| Spray Booth | Booth Hood | a) 200 CFM/ft ² for Face Area Up To 4 ft ² b) 150 CFM/ft ² for Face Area Over 4 ft ² |
| Steam Kettles | Canopy Hood | 150 FPM at Face |
| Varnish Kettles | Canopy Hood | 200-250 FPM at Face |
| Wire Impregnating | Covered Tanks | 200 CFM/ft ² of Opening |

Note: The flow rates and velocities shown in the charts on this page are based on standard air density. For conditions not at standard density such as high temperature, moisture or elevation, convert the operating conditions to standard air conditions using the correction factors found in the Temperature and Altitude Correction Chart on page 4.

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Minimum Duct velocities For Conveying Materials

After the exhaust hood removes the fumes or dust from the work station, the velocity downstream of the hood must be high enough to prevent the material from clogging the ductwork. The velocity downstream of the hood is defined as the *minimum duct velocity* and is determined by the type of material being conveyed through the duct. The table at right shows typical duct velocities for various materials.

| MATERIAL | AVG. VELOCITY TO CONVEY MATERIAL (FPM) |
|--|--|
| VERY FINE LIGHT DUST: Cotton Lint, Wood Flour, Litho Powder | 2500-3000 |
| DRY DUSTS & POWDERS: Fine Rubber Dust, Jute Lint, Cotton Dust, Light Shavings, Soap Dust | 3000-4000 |
| AVERAGE INDUSTRIAL DUST: Grinding Dust, Buffing Lint-Dry, Wool Jute Dust-Shaker Waste, Shoe Dust, Granite Dust, Silica Flour, General Material Handling, Brick Cutting, Clay Dust, Foundry-General, Limestone Dust, Packaging & Weighing Asbestos Dust in Textile Industries | 3500-4000 |
| HEAVY DUSTS Sawdust-Heavy & Wet, Metal Turnings, Foundry Tumbling Barrels & Shake-Out, Sandblast Dust, Wood Blocks, Brass Turnings, Cast Iron Boring Dust, Lead Dust | 4000-4500 |
| HEAVY OR MOIST: Lead Dusts with Small Chips, Moist Cement Dust, Asbestos Chunks From Transite Pipe Cutting Machines, Buffing Lint-Sticky, Quick-Lime Dust | 4500 & Up |

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FAN ENGINEERING WEALTH GUIDE PART I

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Air Change Rates for ventilation

The volume of fresh air (CFM) required to a given area can be easily estimated by the "air change method." This method is recommended for standard commercial type applications where environmental control of hazards, heat and/or odors is not necessary.

Other items to consider when determining the number of air changes required are:

- Local code requirements on air changes.
- How the space is used.
- The type of climate in the area, e.g., hot, moderate or cold.

The air volume (CFM) can be estimated by using the following equation and the chart at right that defines the number of air changes for given area.

$$\text{Volume of Air} = \frac{\text{Room Volume (ft}^3\text{)}}{\text{No. of Air Changes (min./change)}}$$

| AREA TYPE | MINUTES PER CHANGE |
|------------------|--------------------|
| ASSEMBLY HALL | 3-10 |
| BAKERY | 1-3 |
| BAR | 2-4 |
| BOWLING ALLEY | 3-7 |
| BOILER ROOM | 1-3 |
| CAFETERIA | 3-5 |
| CHURCH | 4-10 |
| CLASSROOM | 4-6 |
| ENGINE ROOM | 1-3 |
| FACTORY | 2-7 |
| FORGE SHOP | 1-2 |
| FOUNDRY | 1-5 |
| GENERATOR ROOM | 2-5 |
| HOSPITAL | 4-6 |
| KITCHEN | 2-3 |
| LABORATORY | 2-5 |
| LAUNDRY | 2-4 |
| LOCKER ROOM | 4-15 |
| MACHINE SHOP | 3-6 |
| MILL | 3-8 |
| OFFICE | 2-8 |
| RESTAURANT | 5-10 |
| RETAIL STORE | 5-10 |
| RESTROOM/TOILET | 2-5 |
| TRANSFORMER ROOM | 1-5 |
| WAREHOUSE | 4-10 |

velocity-to-velocity Pressure Conversion Chart

Values based at Standard Density, 0.075lbs/ft³.

Calculated by the formula:

$$VP = \left(\frac{V}{4008.6} \right)^2$$

For other densities use the formula:

$$VP = \left(\frac{V}{1097.8} \right)^2 \times \text{Density}$$

Where:
V is velocity in ft./min.
Density is in lb/ft³.

| V-VELOCITY FPM | VP-VELOCITY PRESSURE IN. WATER | V-VELOCITY FPM | VP-VELOCITY PRESSURE IN. WATER | V-VELOCITY FPM | VP-VELOCITY PRESSURE IN. WATER |
|----------------|--------------------------------|----------------|--------------------------------|----------------|--------------------------------|
| 100 | 0.0006 | 2500 | 0.389 | 4900 | 1.49 |
| 200 | 0.0025 | 2600 | 0.421 | 5000 | 1.56 |
| 300 | 0.0056 | 2700 | 0.454 | 5100 | 1.62 |
| 400 | 0.010 | 2800 | 0.488 | 5200 | 1.68 |
| 500 | 0.016 | 2900 | 0.523 | 5300 | 1.75 |
| 600 | 0.022 | 3000 | 0.560 | 5400 | 1.81 |
| 700 | 0.030 | 3100 | 0.598 | 5500 | 1.88 |
| 800 | 0.040 | 3200 | 0.637 | 5600 | 1.95 |
| 900 | 0.050 | 3300 | 0.678 | 5700 | 2.02 |
| 1000 | 0.062 | 3400 | 0.719 | 5800 | 2.09 |
| 1100 | 0.075 | 3500 | 0.762 | 5900 | 2.17 |
| 1200 | 0.090 | 3600 | 0.807 | 6000 | 2.24 |
| 1300 | 0.105 | 3700 | 0.852 | 6100 | 2.32 |
| 1400 | 0.122 | 3800 | 0.899 | 6200 | 2.39 |
| 1500 | 0.140 | 3900 | 0.947 | 6300 | 2.47 |
| 1600 | 0.159 | 4000 | 1.00 | 6400 | 2.55 |
| 1700 | 0.180 | 4100 | 1.05 | 6500 | 2.63 |
| 1800 | 0.202 | 4200 | 1.10 | 6600 | 2.71 |
| 1900 | 0.225 | 4300 | 1.15 | 6700 | 2.79 |
| 2000 | 0.249 | 4400 | 1.20 | 6800 | 2.88 |
| 2100 | 0.274 | 4500 | 1.26 | 6900 | 2.96 |
| 2200 | 0.301 | 4600 | 1.32 | 7000 | 3.05 |
| 2300 | 0.329 | 4700 | 1.37 | 7100 | 3.14 |
| 2400 | 0.358 | 4800 | 1.43 | 7200 | 3.23 |

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Definitions of English & Metric Units

| | | | | | |
|-----|-------------------------|-----------------|---------------|------|--------------------------|
| °C | = degrees Celsius | in. | = inch | N | = Newton |
| cfm | = cubic feet per minute | kg | = kilogram | Nm | = Newton-meter |
| cm | = centimeter | km | = kilometer | oz. | = ounce |
| °F | = degrees Fahrenheit | kPa | = kilopascal | psi | = pounds per square inch |
| ft | = foot | l | = liter | rpm | = revolutions per minute |
| fpm | = feet per minute | lb. | = pound | rps | = revolutions per second |
| g | = gram | lbf | = pound force | sec. | = second |
| Hg | = mercury | lb _m | = pound mass | W | = Watts |
| hp | = horsepower | m | = meter | wg | = water gauge |
| hpm | = metric horsepower | min. | = minute | | |
| hr. | = hour | mm | = millimeter | | |

Pressure Equivalent Chart

This chart shows pressure values in inches water gauge and the equivalent pressure in other commonly used unit.

| INCHES WATER (IN. WG) | INCHES MERCURY (IN. Hg) | OUNCES PER SQ. IN. (oz./in) ² | POUNDS PER SQ. IN. (lb./in) ² | PASCALS (Pa) | KILOPASCALS (kPa) | MILLIMETERS WATER (mm WG) |
|-----------------------|-------------------------|--|--|--------------|-------------------|---------------------------|
| 1 | 0.0736 | 0.577 | 0.0361 | 249 | 0.25 | 25.4 |
| 2 | 0.1471 | 1.154 | 0.0721 | 498 | 0.50 | 50.8 |
| 3 | 0.2207 | 1.731 | 0.1082 | 747 | 0.75 | 76.2 |
| 4 | 0.2942 | 2.308 | 0.1443 | 996 | 1.00 | 101.6 |
| 5 | 0.3678 | 2.886 | 0.1804 | 1245 | 1.25 | 127.0 |
| 6 | 0.4414 | 3.463 | 0.2164 | 1495 | 1.49 | 152.4 |
| 7 | 0.5149 | 4.040 | 0.2525 | 1744 | 1.74 | 177.8 |
| 8 | 0.5885 | 4.617 | 0.2886 | 1993 | 1.99 | 203.2 |
| 9 | 0.6620 | 5.194 | 0.3246 | 2242 | 2.24 | 228.6 |
| 10 | 0.7356 | 5.771 | 0.3607 | 2491 | 2.49 | 254.0 |
| 11 | 0.8092 | 6.348 | 0.3968 | 2740 | 2.74 | 279.4 |
| 12 | 0.8827 | 6.925 | 0.4328 | 2989 | 2.99 | 304.8 |
| 13 | 0.9563 | 7.503 | 0.4689 | 3238 | 3.24 | 330.2 |
| 14 | 1.0298 | 8.080 | 0.5050 | 3487 | 3.49 | 355.6 |
| 15 | 1.1034 | 8.657 | 0.5411 | 3736 | 3.74 | 381.0 |
| 16 | 1.1770 | 9.234 | 0.5771 | 3985 | 3.99 | 406.4 |
| 17 | 1.2505 | 9.811 | 0.6132 | 4235 | 4.23 | 431.8 |
| 18 | 1.3241 | 10.388 | 0.6493 | 4484 | 4.48 | 457.2 |
| 19 | 1.3976 | 10.965 | 0.6853 | 4733 | 4.73 | 482.6 |
| 20 | 1.4712 | 11.542 | 0.7214 | 4982 | 4.98 | 508.0 |
| 21 | 1.5448 | 12.120 | 0.7575 | 5231 | 5.23 | 533.4 |
| 22 | 1.6183 | 12.697 | 0.7935 | 5480 | 5.48 | 558.8 |
| 23 | 1.6919 | 13.274 | 0.8296 | 5729 | 5.73 | 584.2 |
| 24 | 1.7654 | 13.851 | 0.8657 | 5978 | 5.98 | 609.6 |
| 25 | 1.8390 | 14.428 | 0.9018 | 6227 | 6.23 | 635.0 |
| 26 | 1.9126 | 15.005 | 0.9378 | 6476 | 6.48 | 660.4 |
| 27 | 1.9861 | 15.582 | 0.9739 | 6725 | 6.73 | 685.8 |
| 28 | 2.0597 | 16.159 | 1.0100 | 6974 | 6.97 | 711.2 |
| 29 | 2.1332 | 16.736 | 1.0460 | 7223 | 7.22 | 736.6 |
| 30 | 2.2068 | 17.314 | 1.0821 | 7472 | 7.47 | 762.0 |
| 31 | 2.2804 | 17.891 | 1.1182 | 7721 | 7.72 | 787.4 |
| 32 | 2.3539 | 18.468 | 1.1542 | 7970 | 7.97 | 812.8 |
| 33 | 2.4275 | 19.045 | 1.1903 | 8219 | 8.22 | 838.2 |
| 34 | 2.5010 | 19.622 | 1.2264 | 8468 | 8.47 | 863.6 |
| 35 | 2.5746 | 20.199 | 1.2625 | 8717 | 8.72 | 889.0 |
| 36 | 2.6482 | 20.776 | 1.2985 | 8966 | 8.97 | 914.4 |
| 37 | 2.7217 | 21.353 | 1.3346 | 9215 | 9.22 | 939.8 |
| 38 | 2.7953 | 21.931 | 1.3707 | 9464 | 9.47 | 965.2 |
| 39 | 2.8688 | 22.508 | 1.4067 | 9713 | 9.72 | 990.6 |
| 40 | 2.9424 | 23.085 | 1.4428 | 9962 | 9.97 | 1016.0 |
| 41 | 3.0160 | 23.662 | 1.4789 | 10211 | 10.22 | 1041.4 |
| 42 | 3.0895 | 24.239 | 1.5149 | 10460 | 10.47 | 1066.8 |
| 43 | 3.1631 | 24.816 | 1.5510 | 10709 | 10.72 | 1092.2 |
| 44 | 3.2366 | 25.393 | 1.5871 | 10958 | 10.97 | 1117.6 |
| 45 | 3.3102 | 25.970 | 1.6232 | 11207 | 11.22 | 1143.0 |

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English & Metric Conversions

See page 12 for expanded Temperature Conversion table.

| AREA | | |
|--------------------|-----------------|--------------------|
| MULTIPLY | By | TO OBTAIN |
| in ² | 0.006944 | ft ² |
| | 0.0006452 | m ² |
| ft ² | 645.16 | mm ² |
| | 144 | in ² |
| | 0.09290 | m ² |
| m ² | 92903 | mm ² |
| | 10.76 | ft ² |
| | 1550 | in ² |
| | 10 ⁶ | mm ² |
| DENSITY | | |
| MULTIPLY | By | TO OBTAIN |
| lb/ft ³ | 16.02 | kg/m ³ |
| kg/m ³ | 0.06243 | lb/ft ³ |
| LENGTH | | |
| MULTIPLY | By | TO OBTAIN |
| ft | 12 | in |
| | 0.3048 | m |
| | 304.80 | mm |
| in | 0.0833 | ft |
| | 0.02540 | m |
| m | 25.4 | mm |
| | 3.2808 | ft |
| | 39.37 | in |
| mm | 1000 | mm |
| | 0.003281 | ft |
| | 0.03937 | in |
| | 0.001 | m |
| MASS | | |
| MULTIPLY | By | TO OBTAIN |
| lb _m | 16 | oz |
| | 453.59 | grams |
| oz | 0.45359 | kg |
| | 0.0625 | lb _m |
| grams | 28.35 | grams |
| | 0.0283 | kg |
| | 0.002205 | lb _m |
| kg | 0.03527 | oz |
| | 0.001 | kg |
| | 2.2046 | lb _m |
| | 35.274 | oz |
| | 1000 | grams |
| MOMENT OF INERTIA | | |
| MULTIPLY | By | TO OBTAIN |
| lb-in ² | 0.0069 | lb-ft ² |
| | 0.0002926 | kg-m ² |
| lb-ft ² | 144 | lb-in ² |
| | 0.04214 | kg-m ² |
| kg-m ² | 23.73 | lb-ft ² |
| | 3417.2 | lb-in ² |
| POWER | | |
| MULTIPLY | By | TO OBTAIN |
| HP | 33000 | ft-lb/min |
| | 550 | ft-lb/s |
| | 745.7 | W |
| ft-lb/min | 0.7457 | KW |
| | 76.04 | kg-m/sec |
| | 0.000303 | HP |
| ft-lb/s | 0.0167 | ft-lb/s |
| | 0.0226 | W |
| | 0.0023 | kg-m/sec |
| KW | 0.0018 | HP |
| | 60 | ft-lb/min |
| | 1.3558 | W |
| | 0.1388 | kg-m/sec |

| POWER | | | |
|-------------|--------------------------|-----------|-----------|
| MULTIPLY | By | TO OBTAIN | |
| kg-m/sec | 0.01 | hp | |
| | 434.78 | ft-lb/min | |
| | 7.20 | ft-lb/s | |
| | 9.81 | W | |
| PRESSURE | | | |
| MULTIPLY | By | TO OBTAIN | |
| psi | 27.68 | in-wg | |
| | 2.036 | in-Hg | |
| | 6894.8 | Pa | |
| | 703.07 | mm-wg | |
| | 51.715 | mm-Hg | |
| | 0.06805 | atm | |
| | 68.948 | mbar | |
| | 0.03613 | psi | |
| | 0.07356 | in-Hg | |
| | 249.089 | Pa | |
| in-wg | 25.4 | mm-wg | |
| | 1.8683 | mm-Hg | |
| | 0.002458 | atm | |
| | 2.49089 | mbar | |
| | 0.49115 | psi | |
| | 13.595 | in-wg | |
| | 3386.4 | pa | |
| | 345.31 | mm-wg | |
| | 25.4 | mm-Hg | |
| | 0.03342 | atm | |
| in-Hg | 33.864 | mbar | |
| | 0.000145 | psi | |
| | 0.004015 | in-wg | |
| | 0.0002953 | in-Hg | |
| | 0.10197 | mm-wg | |
| | 0.007501 | mm-Hg | |
| | 0.000098692 | atm | |
| | 0.01 | mbar | |
| | 0.001422 | psi | |
| | 0.03937 | in-wg | |
| mm-wg | 0.002896 | in-Hg | |
| | 9.8067 | Pa | |
| | 0.07356 | mm-Hg | |
| | 0.000096784 | atm | |
| | 0.098067 | mbar | |
| | 0.01934 | psi | |
| | 0.53524 | in-wg | |
| | 0.002896 | in-Hg | |
| | 133.32 | Pa | |
| | mm-Hg | 13.595 | mm-wg |
| 0.001316 | | atm | |
| 1.3332 | | mbar | |
| 14.696 | | psi | |
| 406.78 | | in-wg | |
| 29.921 | | in-Hg | |
| 101325 | | Pa | |
| 10332 | | mm-wg | |
| 760 | | mm-Hg | |
| 1013.25 | | mbar | |
| atm | 0.0145 | psi | |
| | 0.40146 | in-wg | |
| | 0.02953 | in-Hg | |
| | 100 | Pa | |
| | 10.1972 | mm-wg | |
| | 0.75006 | mm-Hg | |
| | 0.000987 | atm | |
| | ROTATING SPEED | | |
| | MULTIPLY | By | TO OBTAIN |
| | RPM | 0.0167 | rps |
| 0.0167 | | Hertz | |
| RPS | 60 | rpm | |
| | 60 | Hz | |
| Hertz | 60 | rpm | |
| | 60 | rps | |
| TEMPERATURE | | | |
| | °F = 9/5 C + 32 | | |
| | °C = 5/9 (F - 32) | | |

| TORQUE | | |
|---------------------|-----------|---------------------|
| MULTIPLY | By | TO OBTAIN |
| lb-in | 0.083 | lb-ft |
| | 0.11298 | N-m |
| lb-ft | 12 | lb-in |
| | 1.3558 | N-m |
| N-m | 0.73756 | lb-ft |
| | 8.8507 | lb-in |
| VELOCITY | | |
| MULTIPLY | By | TO OBTAIN |
| fpm | 0.0167 | fps |
| | .2 | in/sec |
| | 0.005080 | m/s |
| fps | 0.30480 | m/min |
| | 60 | fpm |
| | 12 | in/sec |
| in/sec | 0.30480 | m/s |
| | 18.288 | m/min |
| | 5 | fpm |
| m/s | 0.0833 | fps |
| | 0.02540 | m/s |
| | 1.524 | m/min |
| m/min | 196.85 | fpm |
| | 3.2808 | fps |
| | 39.37 | in/sec |
| m/min | 60 | m/min |
| | 3.2808 | fpm |
| | 0.05468 | fps |
| | 0.65617 | in/sec |
| | 0.0167 | m/s |
| VOLUME | | |
| MULTIPLY | By | TO OBTAIN |
| ft ³ | 1728 | in ³ |
| | 28.317 | l |
| | 0.02832 | m ³ |
| in ³ | 0.000579 | ft ³ |
| | 0.01639 | l |
| | 0.0000164 | m ³ |
| l | 0.03531 | ft ³ |
| | 61.024 | in ³ |
| | 0.001 | m ³ |
| m ³ | 35.315 | ft ³ |
| | 61024 | in ³ |
| | 1000 | l |
| VOLUME FLOW | | |
| MULTIPLY | By | TO OBTAIN |
| CFM | 0.0004719 | m ³ /sec |
| | 0.02832 | m ³ /min |
| | 1.6990 | m ³ /hr |
| | 0.47195 | l/s |
| m ³ /sec | 28.317 | l/min |
| | 2118.9 | CFM |
| | 60 | m ³ /min |
| | 3600 | m ³ /hr |
| m ³ /min | 1000 | l/s |
| | 60000 | l/min |
| | 35.315 | CFM |
| | 0.0167 | m ³ /sec |
| m ³ /hr | 60 | m ³ /hr |
| | 16.667 | l/s |
| | 1000 | l/min |
| | 0.58858 | CFM |
| l/s | 0.0167 | m ³ /min |
| | 0.0003 | m ³ /sec |
| | 0.2778 | l/s |
| | 16.667 | l/min |
| l/min | 2.1189 | CFM |
| | 0.001 | m ³ /sec |
| | 0.06 | m ³ /min |
| | 3.6 | m ³ /hr |
| l/min | 60 | l/min |
| | 0.03531 | CFM |
| | 0.000016 | m ³ /sec |
| | 0.001 | m ³ /min |
| l/min | 0.06 | m ³ /hr |
| | 0.0167 | l/s |

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 9711003363

Friction Loss Per 100 Feet of Round Duct

Data is for duct roughness of 0.0005 feet. If a special duct material is being used, please contact the duct material manufacturer for the friction losses. Friction loss in inches H₂O.

| VEL. | DUCT DIAMETER | | | | | | | | | | | | | |
|------|---------------|-------|-----|-------|------|-------|------|-------|------|------|------|------|------|------|
| | 4" | | 5" | | 6" | | 7" | | 8" | | 10" | | 12" | |
| | CFM | FL | CFM | FL | CFM | FL | CFM | FL | CFM | FL | CFM | FL | CFM | FL |
| 2000 | 175 | 1.85 | 273 | 1.39 | 393 | 1.11 | 535 | 0.92 | 698 | 0.77 | 1091 | 0.59 | 1571 | 0.47 |
| 2200 | 192 | 2.21 | 300 | 1.67 | 432 | 1.33 | 588 | 1.10 | 768 | 0.93 | 1200 | 0.71 | 1728 | 0.56 |
| 2400 | 209 | 2.59 | 327 | 1.97 | 471 | 1.57 | 642 | 1.30 | 838 | 1.10 | 1309 | 0.83 | 1885 | 0.67 |
| 2600 | 227 | 3.04 | 355 | 2.30 | 511 | 1.83 | 695 | 1.51 | 908 | 1.28 | 1418 | 0.97 | 2042 | 0.78 |
| 2800 | 244 | 3.49 | 382 | 2.65 | 550 | 2.11 | 748 | 1.74 | 977 | 1.47 | 1527 | 1.12 | 2199 | 0.90 |
| 3000 | 262 | 4.00 | 409 | 3.02 | 589 | 2.41 | 802 | 1.99 | 1047 | 1.68 | 1636 | 1.28 | 2356 | 1.02 |
| 3200 | 279 | 4.52 | 437 | 3.43 | 628 | 2.72 | 855 | 2.25 | 1117 | 1.91 | 1745 | 1.45 | 2513 | 1.16 |
| 3400 | 297 | 5.10 | 464 | 3.85 | 668 | 3.07 | 909 | 2.53 | 1187 | 2.15 | 1854 | 1.63 | 2670 | 1.30 |
| 3600 | 314 | 5.68 | 491 | 4.30 | 707 | 3.43 | 962 | 2.83 | 1257 | 2.40 | 1963 | 1.82 | 2827 | 1.45 |
| 3800 | 332 | 6.33 | 518 | 4.77 | 746 | 3.80 | 1016 | 3.14 | 1327 | 2.66 | 2073 | 2.02 | 2985 | 1.62 |
| 4000 | 349 | 6.97 | 546 | 5.28 | 786 | 4.21 | 1069 | 3.47 | 1396 | 2.94 | 2182 | 2.23 | 3142 | 1.79 |
| 4200 | 367 | 7.69 | 573 | 5.80 | 825 | 4.62 | 1123 | 3.82 | 1466 | 3.23 | 2291 | 2.46 | 3299 | 1.96 |
| 4400 | 384 | 8.39 | 600 | 6.35 | 864 | 5.05 | 1176 | 4.17 | 1536 | 3.54 | 2400 | 2.69 | 3456 | 2.15 |
| 4600 | 402 | 9.18 | 627 | 6.91 | 903 | 5.51 | 1230 | 4.56 | 1606 | 3.86 | 2509 | 2.93 | 3613 | 2.34 |
| 4800 | 419 | 9.95 | 655 | 7.53 | 943 | 5.99 | 1283 | 4.95 | 1676 | 4.19 | 2618 | 3.18 | 3770 | 2.54 |
| 5000 | 437 | 10.80 | 682 | 8.14 | 982 | 6.49 | 1337 | 5.36 | 1746 | 4.54 | 2727 | 3.45 | 3927 | 2.76 |
| 5200 | 454 | 11.63 | 709 | 8.78 | 1021 | 7.00 | 1390 | 5.78 | 1815 | 4.90 | 2836 | 3.72 | 4084 | 2.97 |
| 5400 | 471 | 12.50 | 737 | 9.47 | 1061 | 7.54 | 1443 | 6.22 | 1885 | 5.27 | 2945 | 4.00 | 4241 | 3.20 |
| 5600 | 489 | 13.45 | 764 | 10.16 | 1100 | 8.10 | 1497 | 6.68 | 1955 | 5.66 | 3054 | 4.30 | 4398 | 3.44 |
| 5800 | 506 | 14.37 | 791 | 10.88 | 1139 | 8.67 | 1550 | 7.15 | 2025 | 6.07 | 3163 | 4.61 | 4555 | 3.68 |
| 6000 | 524 | 15.39 | 818 | 11.62 | 1178 | 9.26 | 1604 | 7.65 | 2095 | 6.48 | 3272 | 4.92 | 4712 | 3.93 |
| 6200 | 541 | 16.38 | 846 | 12.41 | 1218 | 9.88 | 1657 | 8.15 | 2164 | 6.91 | 3381 | 5.25 | 4869 | 4.20 |
| 6400 | 559 | 17.47 | 873 | 13.19 | 1257 | 10.51 | 1711 | 8.68 | 2234 | 7.35 | 3491 | 5.59 | 5027 | 4.47 |
| 6600 | 576 | 18.52 | 900 | 14.00 | 1296 | 11.16 | 1764 | 9.22 | 2304 | 7.81 | 3600 | 5.93 | 5184 | 4.74 |
| 6800 | 594 | 19.68 | 928 | 14.87 | 1336 | 11.84 | 1818 | 9.78 | 2374 | 8.28 | 3709 | 6.29 | 5341 | 5.03 |
| 7000 | 611 | 20.80 | 955 | 15.73 | 1375 | 12.53 | 1871 | 10.34 | 2444 | 8.77 | 3818 | 6.66 | 5498 | 5.32 |

| VEL. | DUCT DIAMETER | | | | | | | | | | | | | |
|------|---------------|------|------|------|-------|------|-------|------|-------|------|-------|------|-------|------|
| | 14" | | 16" | | 18" | | 20" | | 22" | | 24" | | 30" | |
| | CFM | FL | CFM | FL | CFM | FL | CFM | FL | CFM | FL | CFM | FL | CFM | FL |
| 2000 | 2138 | 0.39 | 2793 | 0.33 | 3534 | 0.29 | 4363 | 0.25 | 5280 | 0.22 | 6283 | 0.20 | 9817 | 0.15 |
| 2200 | 2352 | 0.47 | 3072 | 0.40 | 3888 | 0.34 | 4800 | 0.30 | 5808 | 0.27 | 6912 | 0.24 | 10799 | 0.19 |
| 2400 | 2566 | 0.55 | 3351 | 0.47 | 4241 | 0.41 | 5236 | 0.36 | 6336 | 0.32 | 7540 | 0.29 | 11781 | 0.22 |
| 2600 | 2779 | 0.64 | 3630 | 0.55 | 4595 | 0.47 | 5672 | 0.42 | 6863 | 0.37 | 8168 | 0.33 | 12763 | 0.26 |
| 2800 | 2993 | 0.74 | 3910 | 0.63 | 4948 | 0.55 | 6109 | 0.48 | 7391 | 0.43 | 8796 | 0.39 | 13744 | 0.29 |
| 3000 | 3207 | 0.85 | 4189 | 0.72 | 5302 | 0.62 | 6545 | 0.55 | 7919 | 0.49 | 9425 | 0.44 | 14726 | 0.34 |
| 3200 | 3421 | 0.96 | 4468 | 0.82 | 5655 | 0.71 | 6981 | 0.62 | 8447 | 0.55 | 10053 | 0.50 | 15708 | 0.38 |
| 3400 | 3635 | 1.08 | 4747 | 0.92 | 6008 | 0.79 | 7418 | 0.70 | 8975 | 0.62 | 10681 | 0.56 | 16690 | 0.43 |
| 3600 | 3848 | 1.20 | 5027 | 1.02 | 6362 | 0.89 | 7854 | 0.78 | 9503 | 0.70 | 11310 | 0.63 | 17671 | 0.48 |
| 3800 | 4062 | 1.34 | 5306 | 1.14 | 6715 | 0.99 | 8290 | 0.87 | 10031 | 0.77 | 11938 | 0.70 | 18653 | 0.53 |
| 4000 | 4276 | 1.48 | 5585 | 1.26 | 7069 | 1.09 | 8727 | 0.96 | 10559 | 0.85 | 12566 | 0.77 | 19635 | 0.59 |
| 4200 | 4490 | 1.63 | 5864 | 1.38 | 7422 | 1.20 | 9163 | 1.05 | 11087 | 0.94 | 13195 | 0.84 | 20617 | 0.65 |
| 4400 | 4704 | 1.78 | 6144 | 1.51 | 7776 | 1.31 | 9599 | 1.15 | 11615 | 1.03 | 13823 | 0.92 | 21598 | 0.71 |
| 4600 | 4917 | 1.94 | 6423 | 1.65 | 8129 | 1.43 | 10036 | 1.26 | 12143 | 1.12 | 14451 | 1.01 | 22580 | 0.77 |
| 4800 | 5131 | 2.11 | 6702 | 1.79 | 8483 | 1.55 | 10472 | 1.37 | 12671 | 1.22 | 15080 | 1.10 | 23562 | 0.84 |
| 5000 | 5345 | 2.28 | 6982 | 1.94 | 8836 | 1.68 | 10909 | 1.48 | 13199 | 1.32 | 15708 | 1.19 | 24544 | 0.91 |
| 5200 | 5559 | 2.46 | 7261 | 2.09 | 9189 | 1.81 | 11345 | 1.60 | 13727 | 1.42 | 16336 | 1.28 | 25525 | 0.98 |
| 5400 | 5773 | 2.65 | 7540 | 2.25 | 9543 | 1.95 | 11781 | 1.72 | 14255 | 1.53 | 16965 | 1.38 | 26507 | 1.05 |
| 5600 | 5986 | 2.85 | 7819 | 2.42 | 9896 | 2.10 | 12218 | 1.85 | 14783 | 1.64 | 17593 | 1.48 | 27489 | 1.13 |
| 5800 | 6200 | 3.05 | 8099 | 2.59 | 10250 | 2.25 | 12654 | 1.98 | 15311 | 1.76 | 18221 | 1.58 | 28470 | 1.21 |
| 6000 | 6414 | 3.26 | 8378 | 2.77 | 10603 | 2.40 | 13090 | 2.11 | 15839 | 1.88 | 18850 | 1.69 | 29452 | 1.29 |
| 6200 | 6628 | 3.48 | 8657 | 2.95 | 10957 | 2.56 | 13527 | 2.25 | 16367 | 2.01 | 19478 | 1.81 | 30434 | 1.38 |
| 6400 | 6842 | 3.70 | 8936 | 3.14 | 11310 | 2.72 | 13963 | 2.40 | 16895 | 2.14 | 20106 | 1.92 | 31416 | 1.47 |
| 6600 | 7055 | 3.93 | 9216 | 3.34 | 11664 | 2.89 | 14399 | 2.55 | 17423 | 2.27 | 20735 | 2.04 | 32397 | 1.56 |
| 6800 | 7269 | 4.16 | 9495 | 3.54 | 12017 | 3.07 | 14836 | 2.70 | 17951 | 2.40 | 21363 | 2.16 | 33379 | 1.65 |
| 7000 | 7483 | 4.41 | 9774 | 3.75 | 12370 | 3.25 | 15272 | 2.86 | 18479 | 2.55 | 21991 | 2.29 | 34361 | 1.75 |

Ventech Systems Private Limi ted

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Works : Plot No. B-13, Sector A-5/6, Tronica City, Loni - 201102, Ghaziabad (U.P.), India, Tel.: 09711003363

Area and Circumference of Circles

| DIA. (IN.) | AREA | | CIRCUM-FERENCE | |
|------------|-----------------|-----------------|----------------|-------|
| | IN ² | FT ² | IN | FT |
| 1 | 0.785 | 0.005 | 3.14 | 0.262 |
| 2 | 3.14 | 0.022 | 6.28 | 0.523 |
| 3 | 7.07 | 0.049 | 9.42 | 0.785 |
| 4 | 12.57 | 0.087 | 12.57 | 1.054 |
| 5 | 19.63 | 0.136 | 15.71 | 1.31 |
| 6 | 28.27 | 0.196 | 18.85 | 1.57 |
| 7 | 38.48 | 0.267 | 21.99 | 1.83 |
| 8 | 50.27 | 0.349 | 25.13 | 2.09 |
| 9 | 63.62 | 0.441 | 28.27 | 2.36 |
| 10 | 78.54 | 0.545 | 31.42 | 2.62 |
| 11 | 95.03 | 0.659 | 34.56 | 2.88 |
| 12 | 113.00 | 0.785 | 37.70 | 3.14 |
| 13 | 133.00 | 0.921 | 40.84 | 3.40 |
| 14 | 154.00 | 1.07 | 43.98 | 3.66 |
| 15 | 177.00 | 1.23 | 47.12 | 3.93 |
| 16 | 201.00 | 1.40 | 50.27 | 4.19 |
| 17 | 227.00 | 1.57 | 53.41 | 4.45 |
| 18 | 254.00 | 1.77 | 56.55 | 4.71 |
| 19 | 284.00 | 1.97 | 59.69 | 4.97 |
| 20 | 314.00 | 2.18 | 62.83 | 5.23 |
| 21 | 346.00 | 2.40 | 65.97 | 5.50 |
| 22 | 380.00 | 2.64 | 69.12 | 5.76 |
| 23 | 415.00 | 2.88 | 72.26 | 6.02 |
| 24 | 452.00 | 3.14 | 75.40 | 6.28 |
| 25 | 491.00 | 3.41 | 78.54 | 6.54 |
| 26 | 531.00 | 3.68 | 81.68 | 6.80 |
| 27 | 573.00 | 3.97 | 84.82 | 7.07 |
| 28 | 616.00 | 4.27 | 87.96 | 7.33 |
| 29 | 661.00 | 4.58 | 91.11 | 7.59 |
| 30 | 707.00 | 4.90 | 94.25 | 7.85 |
| 31 | 755.00 | 5.24 | 97.39 | 8.11 |
| 32 | 804.00 | 5.58 | 100.53 | 8.37 |
| 33 | 855.00 | 5.93 | 103.67 | 8.64 |
| 34 | 908.00 | 6.30 | 106.81 | 8.90 |

| DIA. (IN.) | AREA | | CIRCUM-FERENCE | |
|------------|-----------------|-----------------|----------------|-------|
| | IN ² | FT ² | IN | FT |
| 35 | 962 | 6.68 | 109.96 | 9.16 |
| 36 | 1018 | 7.06 | 113.10 | 9.42 |
| 37 | 1075 | 7.46 | 116.24 | 9.68 |
| 38 | 1134 | 7.87 | 119.38 | 9.94 |
| 39 | 1195 | 8.29 | 122.52 | 10.21 |
| 40 | 1257 | 8.72 | 125.66 | 10.47 |
| 41 | 1320 | 9.16 | 128.81 | 10.73 |
| 42 | 1385 | 9.61 | 131.95 | 10.99 |
| 43 | 1452 | 10.08 | 135.09 | 11.25 |
| 44 | 1521 | 10.55 | 138.23 | 11.51 |
| 45 | 1590 | 11.04 | 141.37 | 11.78 |
| 46 | 1662 | 11.53 | 144.51 | 12.04 |
| 47 | 1735 | 12.04 | 147.65 | 12.30 |
| 48 | 1810 | 12.56 | 150.80 | 12.56 |
| 49 | 1886 | 13.08 | 153.94 | 12.82 |
| 50 | 1963 | 13.62 | 157.08 | 13.08 |
| 51 | 2043 | 14.17 | 160.22 | 13.35 |
| 52 | 2124 | 14.74 | 163.36 | 13.61 |
| 53 | 2206 | 15.31 | 166.50 | 13.87 |
| 54 | 2290 | 15.89 | 169.65 | 14.13 |
| 55 | 2376 | 16.49 | 172.79 | 14.39 |
| 56 | 2463 | 17.09 | 175.93 | 14.65 |
| 57 | 2552 | 17.71 | 179.07 | 14.92 |
| 58 | 2642 | 18.33 | 182.21 | 15.18 |
| 59 | 2734 | 18.97 | 185.35 | 15.44 |
| 60 | 2827 | 19.62 | 188.50 | 15.70 |
| 61 | 2922 | 20.28 | 191.64 | 15.96 |
| 62 | 3019 | 20.95 | 194.78 | 16.23 |
| 63 | 3117 | 21.63 | 197.92 | 16.49 |
| 64 | 3217 | 22.32 | 201.06 | 16.75 |
| 65 | 3318 | 23.03 | 204.20 | 17.01 |
| 66 | 3421 | 23.74 | 207.35 | 17.27 |
| 67 | 3526 | 24.46 | 210.49 | 17.53 |
| 68 | 3632 | 25.20 | 213.63 | 17.80 |

| DIA. (IN.) | AREA | | CIRCUM-FERENCE | |
|------------|-----------------|-----------------|----------------|-------|
| | IN ² | FT ² | IN | FT |
| 69 | 3739 | 25.95 | 216.77 | 18.06 |
| 70 | 3848 | 26.70 | 219.91 | 18.32 |
| 71 | 3959 | 27.47 | 223.05 | 18.58 |
| 72 | 4072 | 28.25 | 226.19 | 18.84 |
| 73 | 4185 | 29.04 | 229.34 | 19.10 |
| 74 | 4301 | 29.84 | 232.48 | 19.37 |
| 75 | 4418 | 30.66 | 235.62 | 19.63 |
| 76 | 4536 | 31.48 | 238.76 | 19.89 |
| 77 | 4657 | 32.31 | 241.90 | 20.15 |
| 78 | 4778 | 33.16 | 245.04 | 20.41 |
| 79 | 4902 | 34.01 | 248.19 | 20.67 |
| 80 | 5027 | 34.88 | 251.33 | 20.94 |
| 81 | 5153 | 35.76 | 254.47 | 21.20 |
| 82 | 5281 | 36.64 | 257.61 | 21.46 |
| 83 | 5411 | 37.54 | 260.75 | 21.72 |
| 84 | 5542 | 38.45 | 263.89 | 21.98 |
| 85 | 5675 | 39.37 | 267.04 | 22.24 |
| 86 | 5809 | 40.31 | 270.18 | 22.51 |
| 87 | 5945 | 41.25 | 273.32 | 22.77 |
| 88 | 6082 | 42.20 | 276.46 | 23.03 |
| 89 | 6221 | 43.17 | 279.60 | 23.29 |
| 90 | 6362 | 44.14 | 282.74 | 23.55 |
| 91 | 6504 | 45.13 | 285.88 | 23.81 |
| 92 | 6648 | 46.13 | 289.03 | 24.08 |
| 93 | 6793 | 47.14 | 292.17 | 24.34 |
| 94 | 6940 | 48.15 | 295.31 | 24.60 |
| 95 | 7088 | 49.18 | 298.45 | 24.86 |
| 96 | 7238 | 50.23 | 301.59 | 25.12 |
| 97 | 7390 | 51.28 | 304.73 | 25.38 |
| 98 | 7543 | 52.34 | 307.88 | 25.65 |
| 99 | 7698 | 53.41 | 311.02 | 25.91 |
| 100 | 7854 | 54.50 | 314.16 | 26.17 |

Equations: Area = πr^2 (r = radius of circle)
Circumference = $2\pi r$ or πd (r = radius of circle; d = diameter of circle)

Gauges & Equivalent Metal Thickness

Steel Sheet Gauges & Weights

| GAUGE | | | | |
|-------|-------|---------|--------|---------|
| 1" | 1 | 25.4000 | 41.829 | 204.379 |
| 3/4" | 3/4 | 19.0500 | 31.372 | 153.280 |
| 5/8" | 5/8 | 15.8750 | 26.143 | 127.73 |
| 1/2" | 1/2 | 12.7000 | 20.915 | 102.187 |
| 3/8" | 3/8 | 9.5250 | 15.686 | 76.640 |
| 5/16" | 5/16 | 7.9375 | 13.072 | 63.867 |
| 1/4" | 1/4 | 6.3500 | 10.457 | 51.093 |
| 3/16" | 3/16 | 4.7625 | 7.843 | 38.320 |
| 7 | .1793 | 4.5542 | 7.500 | 36.644 |
| 8 | .1644 | 4.1758 | 6.875 | 33.591 |
| 9 | .1495 | 3.7973 | 6.250 | 30.537 |
| 10 | .1345 | 3.4163 | 5.625 | 27.483 |
| 11 | .1196 | 3.0378 | 5.000 | 24.429 |
| 12 | .1046 | 2.6568 | 4.375 | 21.376 |
| 13 | .0897 | 2.2784 | 3.750 | 18.322 |
| 14 | .0747 | 1.8974 | 3.125 | 15.268 |
| 15 | .0673 | 1.7094 | 2.813 | 13.744 |
| 16 | .0598 | 1.5189 | 2.500 | 12.215 |
| 17 | .0538 | 1.3665 | 2.250 | 10.993 |
| 18 | .0478 | 1.2141 | 2.000 | 9.772 |
| 19 | .0418 | 1.0617 | 1.750 | 8.550 |
| 20 | .0359 | 0.9119 | 1.500 | 7.329 |
| 21 | .0329 | 0.8357 | 1.375 | 6.718 |
| 22 | .0299 | 0.7595 | 1.250 | 6.107 |
| 23 | .0269 | 0.6833 | 1.125 | 5.497 |
| 24 | .0239 | 0.6071 | 1.000 | 4.886 |
| 25 | .0209 | 0.5309 | 0.875 | 4.275 |
| 26 | .0179 | 0.4547 | 0.750 | 3.664 |
| 27 | .0164 | 0.4166 | 0.688 | 3.361 |

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Fractions to Equivalent Decimal values

| FRACTION | DECIMAL |
|-----------------|---------|
| $\frac{1}{64}$ | .016 |
| $\frac{1}{32}$ | .031 |
| $\frac{3}{64}$ | .047 |
| $\frac{1}{16}$ | .063 |
| $\frac{5}{64}$ | .078 |
| $\frac{3}{32}$ | .094 |
| $\frac{1}{64}$ | .109 |
| $\frac{1}{8}$ | .125 |
| $\frac{9}{64}$ | .141 |
| $\frac{5}{32}$ | .156 |
| $\frac{11}{64}$ | .172 |
| $\frac{3}{16}$ | .188 |
| $\frac{13}{64}$ | .203 |
| $\frac{1}{32}$ | .219 |
| $\frac{15}{64}$ | .234 |
| $\frac{1}{4}$ | .250 |
| $\frac{17}{64}$ | .266 |
| $\frac{9}{32}$ | .281 |
| $\frac{19}{64}$ | .307 |
| $\frac{5}{16}$ | .313 |
| $\frac{21}{64}$ | .328 |
| $\frac{11}{32}$ | .344 |

| FRACTION | DECIMAL |
|-----------------|---------|
| $\frac{23}{64}$ | .359 |
| $\frac{3}{8}$ | .375 |
| $\frac{25}{64}$ | .391 |
| $\frac{13}{32}$ | .406 |
| $\frac{27}{64}$ | .422 |
| $\frac{1}{16}$ | .438 |
| $\frac{29}{64}$ | .453 |
| $\frac{15}{32}$ | .469 |
| $\frac{31}{64}$ | .484 |
| $\frac{1}{2}$ | .500 |
| $\frac{33}{64}$ | .516 |
| $\frac{17}{32}$ | .531 |
| $\frac{35}{64}$ | .547 |
| $\frac{9}{16}$ | .563 |
| $\frac{37}{64}$ | .578 |
| $\frac{19}{32}$ | .594 |
| $\frac{39}{64}$ | .609 |
| $\frac{5}{8}$ | .625 |
| $\frac{41}{64}$ | .641 |
| $\frac{21}{32}$ | .656 |
| $\frac{43}{64}$ | .672 |
| $\frac{11}{16}$ | .688 |

| FRACTION | DECIMAL |
|-----------------|---------|
| $\frac{45}{64}$ | .703 |
| $\frac{23}{32}$ | .719 |
| $\frac{47}{64}$ | .734 |
| $\frac{3}{4}$ | .750 |
| $\frac{49}{64}$ | .766 |
| $\frac{25}{32}$ | .781 |
| $\frac{51}{64}$ | .797 |
| $\frac{13}{16}$ | .813 |
| $\frac{53}{64}$ | .828 |
| $\frac{27}{32}$ | .844 |
| $\frac{55}{64}$ | .859 |
| $\frac{1}{8}$ | .875 |
| $\frac{57}{64}$ | .861 |
| $\frac{29}{32}$ | .906 |
| $\frac{59}{64}$ | .922 |
| $\frac{15}{16}$ | .938 |
| $\frac{61}{64}$ | .953 |
| $\frac{31}{32}$ | .969 |
| $\frac{63}{64}$ | .984 |
| 1 | 1.00 |

Temperature Conversions

| °C | °F | °C | °F | °C | °F | °C | °F | °C | °F | °C | °F |
|-----|-------|----|------|----|-------|-----|-------|-----|-----|-----|------|
| -40 | -40.0 | -2 | 28.4 | 36 | 96.8 | 74 | 165.2 | 160 | 320 | 350 | 662 |
| -39 | -38.2 | -1 | 30.2 | 37 | 98.6 | 75 | 167.0 | 165 | 329 | 355 | 671 |
| -38 | -36.4 | 0 | 32.0 | 38 | 100.4 | 76 | 168.8 | 170 | 338 | 360 | 680 |
| -37 | -34.6 | 1 | 33.8 | 39 | 102.2 | 77 | 170.6 | 175 | 347 | 365 | 689 |
| -36 | -32.8 | 2 | 35.6 | 40 | 104.0 | 78 | 172.4 | 180 | 356 | 370 | 698 |
| -35 | -31.0 | 3 | 37.4 | 41 | 105.8 | 79 | 174.2 | 185 | 365 | 375 | 707 |
| -34 | -29.2 | 4 | 39.2 | 42 | 107.6 | 80 | 176.0 | 190 | 374 | 380 | 716 |
| -33 | -27.4 | 5 | 41.0 | 43 | 109.4 | 81 | 177.8 | 195 | 383 | 385 | 725 |
| -32 | -25.6 | 6 | 42.8 | 44 | 111.2 | 82 | 179.6 | 200 | 392 | 390 | 734 |
| -31 | -23.8 | 7 | 44.6 | 45 | 113.0 | 83 | 181.4 | 205 | 401 | 395 | 743 |
| -30 | -22.0 | 8 | 46.4 | 46 | 114.8 | 84 | 183.2 | 210 | 410 | 400 | 752 |
| -29 | -20.2 | 9 | 48.2 | 47 | 116.6 | 85 | 185.0 | 215 | 419 | 410 | 770 |
| -28 | -18.4 | 10 | 50.0 | 48 | 118.4 | 86 | 186.8 | 220 | 428 | 420 | 788 |
| -27 | -16.6 | 11 | 51.8 | 49 | 120.2 | 87 | 188.6 | 225 | 437 | 430 | 806 |
| -26 | -14.8 | 12 | 53.6 | 50 | 122.0 | 88 | 190.4 | 230 | 446 | 440 | 824 |
| -25 | -13.0 | 13 | 55.4 | 51 | 123.8 | 89 | 192.2 | 235 | 455 | 450 | 842 |
| -24 | -11.2 | 14 | 57.2 | 52 | 125.6 | 90 | 194.0 | 240 | 464 | 460 | 860 |
| -23 | -9.4 | 15 | 59.0 | 53 | 127.4 | 91 | 195.8 | 245 | 473 | 470 | 878 |
| -22 | -7.6 | 16 | 60.8 | 54 | 129.2 | 92 | 197.6 | 250 | 482 | 480 | 896 |
| -21 | -5.8 | 17 | 62.6 | 55 | 131.0 | 93 | 199.4 | 255 | 491 | 490 | 914 |
| -20 | -4.0 | 18 | 64.4 | 56 | 132.8 | 94 | 201.2 | 260 | 500 | 500 | 932 |
| -19 | -2.2 | 19 | 66.2 | 57 | 134.6 | 95 | 203.0 | 265 | 509 | 510 | 950 |
| -18 | -0.4 | 20 | 68.0 | 58 | 136.4 | 96 | 204.8 | 270 | 518 | 520 | 968 |
| -17 | 1.4 | 21 | 69.8 | 59 | 138.2 | 97 | 206.6 | 275 | 527 | 530 | 986 |
| -16 | 3.2 | 22 | 71.6 | 60 | 140.0 | 98 | 208.4 | 280 | 536 | 540 | 1004 |
| -15 | 5.0 | 23 | 73.4 | 61 | 141.8 | 99 | 210.2 | 285 | 545 | 550 | 1022 |
| -14 | 6.8 | 24 | 75.2 | 62 | 143.6 | 100 | 212.0 | 290 | 554 | 560 | 1040 |
| -13 | 8.6 | 25 | 77.0 | 63 | 145.4 | 105 | 221.0 | 295 | 563 | 570 | 1058 |
| -12 | 10.4 | 26 | 78.8 | 64 | 147.2 | 110 | 230.0 | 300 | 572 | 580 | 1076 |
| -11 | 12.2 | 27 | 80.6 | 65 | 149.0 | 115 | 239.0 | 305 | 581 | 590 | 1094 |
| -10 | 14.4 | 28 | 82.4 | 66 | 150.8 | 120 | 248.0 | 310 | 590 | 600 | 1112 |
| -9 | 15.8 | 29 | 84.2 | 67 | 152.6 | 125 | 257.0 | 315 | 599 | 650 | 1202 |
| -8 | 17.6 | 30 | 86.0 | 68 | 154.4 | 130 | 266.0 | 320 | 608 | 700 | 1292 |
| -7 | 19.4 | 31 | 87.8 | 69 | 156.2 | 135 | 275.0 | 325 | 617 | 750 | 1382 |
| -6 | 21.2 | 32 | 89.6 | 70 | 158.0 | 140 | 284.0 | 330 | 626 | 800 | 1472 |
| -5 | 23.0 | 33 | 91.4 | 71 | 159.8 | 145 | 293.0 | 335 | 635 | | |
| -4 | 24.8 | 34 | 93.2 | 72 | 161.6 | 150 | 302.0 | 340 | 644 | | |
| -3 | 26.6 | 35 | 95.0 | 73 | 163.4 | 155 | 311.0 | 345 | 653 | | |